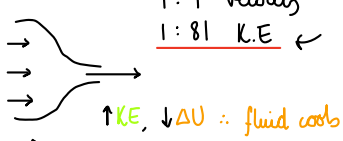


$C = \text{velocity}$

$\dot{m} = \rho AC$  e.g.

3:1 diameter  
9:1 area  
1:9 velocity  
1:81 K.E



Nozzle  
(Accelerates gas)

Assume no W or Q transfer

Diffuser  
(decelerates gas)

$$\dot{Q} + \dot{W} = \dot{m} \left[ (h_2 + \frac{1}{2}c_2^2 + gz_2) - (h_1 + \frac{1}{2}c_1^2 + gz_1) \right]$$

no change in GPE  $\approx$  (horz.)

$$h_2 = h_1 + \frac{c_2^2 - c_1^2}{2}$$

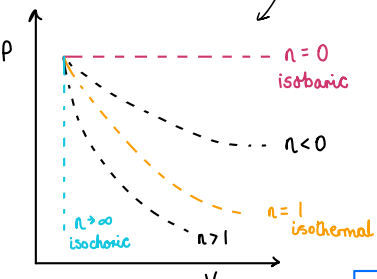
$$h = c_p(T - T_0)$$

$$T_2 = T_1 + \frac{(c_2^2 - c_1^2)}{2c_p}$$

Using ideal gas law equations and  $pV^n = \text{constant}$

$$\left(\frac{mRT}{V}\right)V^n = \text{constant}$$

$$TV^{n-1} = \text{constant}$$

$$\rightarrow T = \text{constant } p^{\frac{n-1}{n}}$$


$n = \gamma$   
isentropic

any other  $n$  not isothermal,  $T_2 \neq T_1$   
 $Q \neq 0, W \neq 0$

**Polytropic Process** ( $pV^n$ )  
(interchange of both work and heat between system and surroundings)

$pV^n = \text{constant}$

$$p_1 V_1^n = p_2 V_2^n$$

$$W_b = \frac{p_2 V_2 - p_1 V_1}{n - 1}$$

and

$$W_b = \frac{mR(T_2 - T_1)}{n - 1}$$

$pV^\gamma = \text{constant}$   
 $p = cV^{-\gamma}$

$$W_b = -\int_1^2 cV^{-\gamma} dV$$

$$W_b = -\frac{[cV^{-\gamma+1}]_1^2}{1-\gamma}$$

$$W_b = \frac{[cV^{-\gamma}V]_1^2}{\gamma-1} = \frac{[pV]_1^2}{\gamma-1} = \frac{p_2 V_2 - p_1 V_1}{\gamma-1}$$

$\gamma = \text{specific capacity ratio}$

**Isentropic Process** ( $pV^\gamma$ )

→ No friction  
→ No heat transfer (adiabatic)

$$W = U_2 - U_1 - Q$$

$$W = mC_v(T_2 - T_1)$$

Replacing T with P and V from  $T = \frac{pV}{mR}$

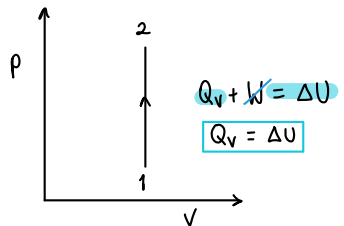
$$W = \frac{m}{m} \left( \frac{C_v}{R} (p_2 V_2 - p_1 V_1) \right)$$

$$\frac{C_v}{R} = \frac{C_v}{C_p - C_v} = \frac{1}{\frac{C_p}{C_v} - 1}$$

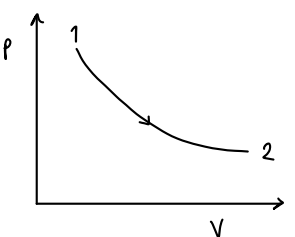
$$\frac{C_p}{C_v} = \gamma \rightarrow \frac{C_v}{R} = \frac{1}{\gamma - 1}$$

$$W = \frac{p_2 V_2 - p_1 V_1}{\gamma - 1}$$

**Constant Volume (Isochoric)**



**Constant Temperature (Isothermal)**



$\Delta U = 0$   
 $0 = Q - W$   
 $Q = W$

$$W = -\int_1^2 p dv = -mRT \int_1^2 \frac{dv}{v}$$

$$= -mRT \ln \left( \frac{V_2}{V_1} \right)$$

$$= -p_1 V_1 \ln \left( \frac{V_2}{V_1} \right)$$

$$= -p_2 V_2 \ln \left( \frac{V_2}{V_1} \right)$$

obtained as  $\int_{V_1}^{V_2} \frac{dv}{v} = \int_{V_1}^{V_2} \frac{1}{v} dv = [\ln v]_{V_1}^{V_2}$

$$= \ln V_2 - \ln V_1 = \ln \left( \frac{V_2}{V_1} \right)$$

# Material and Energy Balances

## Steady Flow

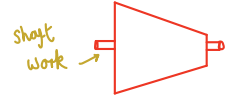
- fluid continuously passes into and away from system  
→ open system

$$\delta Q + \delta W = \delta m \left[ (h_2 + \frac{1}{2}c_2^2 + gz_2) - (h_1 + \frac{1}{2}c_1^2 + gz_1) \right]$$

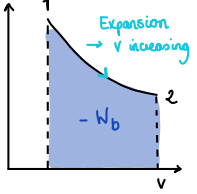
∴ if you have  $\Delta h, KE, PE$   
→  $W + Q$  done/transferred

**Compressor**

- applies work to raise pressure  
→  $\uparrow T$  follows

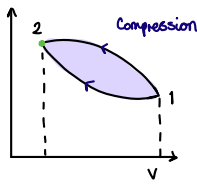


$\dot{Q} = 0$  ← adiabatic



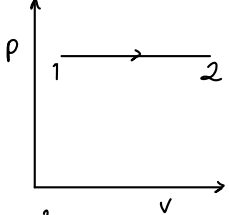
$$W_b = -\int_1^2 p dv$$

-ve as it's expansion  
→  $W$  done on surroundings



Difference in work  
Same final state, different work independent

**Constant Pressure (Isobaric)**

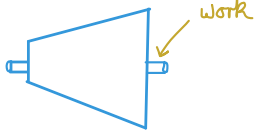


$$-p \int_1^2 dv = -p(V_2 - V_1)$$

$Q_p = \Delta U - W$  (constant)  
 $Q_p = \Delta U + p \Delta V$   
 $Q_p = \Delta(u + pv)$   
 $Q_p = \Delta H$

**Turbine**

- Produces useful work from hot, high pressure gas  
→ exits cold, low pressure



$$\dot{Q} + \dot{W} = \dot{m} \left[ (h_2 + \frac{1}{2}c_2^2 + gz_2) - (h_1 + \frac{1}{2}c_1^2 + gz_1) \right]$$

$h = c_p(T - T_0)$

$$W = \dot{m} \left[ c_p(T_2 - T_1) + \frac{(c_2^2 - c_1^2)}{2} \right]$$

$h$  energy that could be harnessed  
K.E losses

Shaft Work:  
Work done to rotate shaft connected to system: produces torque

Mechanical power =  $\frac{\delta W}{\delta t}$   
mass flow rate =  $\frac{\delta m}{\delta t}$

heating power =  $\frac{\delta Q}{\delta t}$

if relative KE so small for diffuser it can be removed from SFEE

enthalpy  
K.E  
P.E